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### (54) Fuel cell system combustor

(57) A fuel cell system including a fuel reformer heated by a catalytic combustor fired by anode and cathode effluents. The combustor includes a turbulator section at its input end for intimately mixing the anode and cathode effluents before they contact the combustor's primary catalyst bed. The turbulator comprises at

least one porous bed of mixing media that provides a tortuous path therethrough for creating turbulent flow and intimate mixing of the anode and cathode effluents therein.

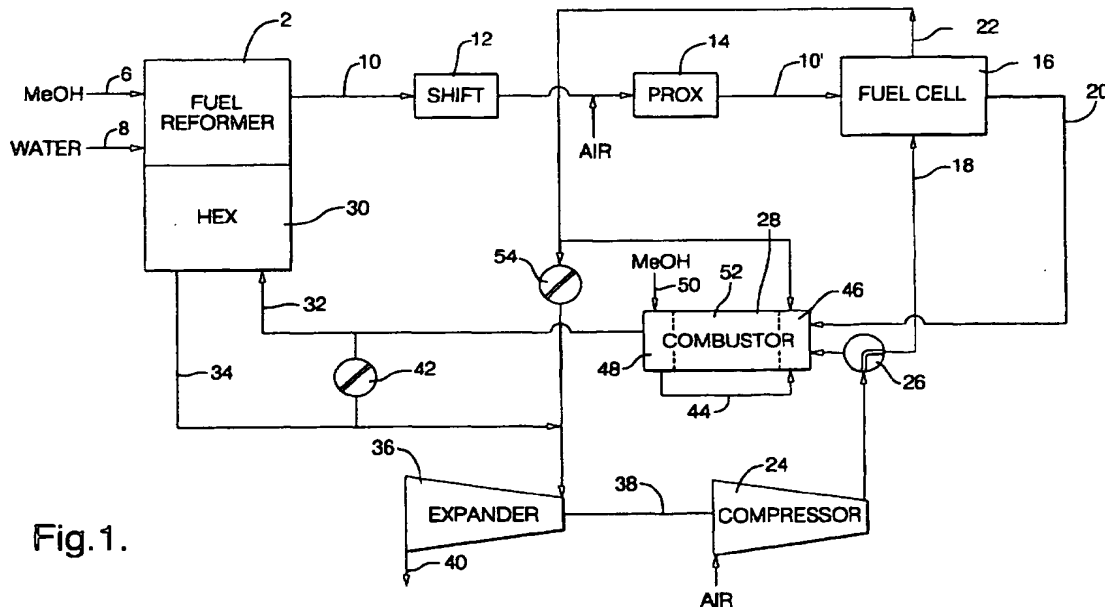


Fig.1.

## Description

[0001] The Government of the United States of America has rights in this invention pursuant to Agreement No. DE-AC02-90CH10435 awarded by the U.S. Department of Energy.

## TECHNICAL FIELD

[0002] The present invention relates to a fuel cell system having a catalytic combustor for heating a fuel reformer, and more particularly to a combustor having a turbulator at the input end thereof.

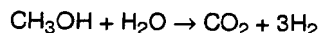
## BACKGROUND OF THE INVENTION

[0003] H<sub>2</sub>-O<sub>2</sub> (air) fuel cells are well known in the art and have been proposed as a power source for many applications. There are several different types of H<sub>2</sub>-O<sub>2</sub> fuel cells including acid-type, alkaline-type, molten-carbonate-type and solid-oxide-type. So-called PEM (proton exchange membrane) fuel cells [a.k.a. SPE (solid polymer electrolyte) fuel cells] are of the acid-type, potentially have high power and low weight, and accordingly are desirable for mobile applications (e.g., electric vehicles). PEM fuel cells are well known in the art, and include a "membrane electrode assembly" (a.k.a. MEA) comprising a thin, proton transmissive, solid polymer membrane-electrolyte having an anode on one of its faces and a cathode on the opposite face. The MEA is sandwiched between a pair of electrically conductive elements which (1) serve as current collectors for the anode and cathode, and (2) contain appropriate channels and/or openings therein for distributing the fuel cell's gaseous reactants over the surfaces of the respective anode and cathode catalysts. A plurality of individual cells are commonly bundled together to form a PEM fuel cell stack.

[0004] In PEM fuel cells hydrogen is the anode reactant (i.e., fuel) and oxygen is the cathode reactant (i.e., oxidant). The oxygen can either be in a pure form (i.e., O<sub>2</sub>), or air (i.e., O<sub>2</sub> admixed with N<sub>2</sub>). The solid polymer electrolytes are typically made from ion exchange resins such as perfluoronated sulfonic acid. The anode/cathode typically comprise finely divided catalytic particles (often supported on carbon particles) admixed with proton conductive resin.

[0005] For vehicular applications, it is desirable to use a liquid fuel such as a low molecular weight alcohol (e.g., methanol or ethanol), or hydrocarbons (e.g., gasoline) as the fuel for the vehicle owing to the ease of onboard storage of liquid fuels and the existence of a nationwide infrastructure for supplying liquid fuels. However, such fuels must be dissociated to release the hydrogen content thereof for fueling the fuel cell. The dissociation reaction is accomplished heterogeneously within a chemical fuel processor, known as a reformer, that provides thermal energy throughout a catalyst

mass and yields a reformat gas comprising primarily hydrogen and carbon dioxide. For example, in the steam methanol reformation process, methanol and water (as steam) are ideally reacted to generate hydrogen and carbon dioxide according to the reaction:



[0006] The reforming reaction is an endothermic reaction that requires external heat for the reaction to occur. Heating the reformer with heat generated externally from either a flame combustor or a catalytic combustor is known. The present invention relates to an improved catalytic combustor, and the integration thereof with a fuel cell system, wherein the combustor is fueled with hydrogen-containing anode effluent and oxygen-containing cathode effluent, and includes means at its input end to induce intimate mixing of the anode effluent with the oxygen-dilute cathode effluent to ensure efficient and uniform burning of the hydrogen on the catalyst bed without the creation of "hot spots" or significant temperature differences throughout the catalyst bed.

## SUMMARY OF THE INVENTION

[0007] The present invention involves a fuel cell system having (a) a stack of H<sub>2</sub>-O<sub>2</sub> fuel cells discharging an H<sub>2</sub>-containing anode effluent and an O<sub>2</sub>-containing cathode effluent, (b) a fuel reformer for converting a hydrogen-containing fuel selected from the group consisting of alcohols and hydrocarbons to H<sub>2</sub> for fueling said cells, and (c) a combustor for heating said fuel reformer. The present invention contemplates an improved catalytic combustor which is fueled by the anode and cathode effluents and includes a turbulator section at its entrance for intimately mixing the anode and cathode effluents. More specifically, the combustor comprises a housing having (1) an input chamber that receives and initially roughly combines the anode and cathode effluents together into a burnable mixture, (2) an exhaust outlet emitting hot combustor exhaust gas to the reformer, (3) a catalyst bed intermediate the input chamber and exhaust outlet for burning the mixture to generate the hot combustor exhaust gas, and (4) a turbulator intermediate the input chamber and the catalyst bed for inducing turbulent mixing of the mixture before it contacts the catalyst bed. The turbulator comprises at least one porous bed having a leading face admitting the mixture into the porous bed from the input chamber, and a trailing face through which the mixture exits the porous bed. A mixing zone intermediate the leading and trailing faces intimately mixes the effluents in the mixture to provide a homogeneous mixture for even burning throughout the catalyst bed. The mixing zone comprises a porous material that defines a multiplicity of tortuously pathed channels through which the reaction mixture passes. Preferably, the turbulator has at least two porous beds arranged in series (i.e., in the direction of

flow) between the input chamber and the catalyst bed. Most preferably, the porous beds will have different porosity profiles, and be separated one from the next by an open space which serves as a mixing confluence for the several streams exiting the many channels through the first mixing media bed. The first porous bed in the direction of flow will preferably have a finer (i.e., smaller pores) porosity profile than the second porous bed.

[0008] The porous beds may comprise a variety of corrosion and heat resistant materials, such as ceramics or refractory metals, and take many different forms so long as they provide a multiplicity of tortuously pathed flow channels therethrough. For example in one embodiment, the porous beds may comprise a stack of fine screens wherein the openings in one screen are offset from openings in adjacent screens to provide the desired tortuous path through the porous bed. Open cell metal foams may also be used. In preferred embodiment, the porous bed comprises a ceramic foam. Most preferably, the ceramic foam has a porosity profile of about 25 pores per lineal inch to about 80 pores per lineal inch. Silicon carbide and yttria-zirconia-aluminum ( $Y_2O_3/ZrO_2/Al_2O_3$ ) have proven to be effective ceramics for applications that see temperatures as high as 700°C. Potentially alternative materials include alumina ( $Al_2O_3$ ), zirconia-alumina ( $ZrO_2/Al_2O_3$ ), partially stabilized zirconia ( $ZrO_2/CaO/MgO$ ), partially stabilized zirconia-magnesia ( $ZrO_2/MgO$ ), partially stabilized zirconia-yttria ( $ZrO_2/Y_2O_3$ ), *inter alia* depending on the temperature and strength requirements of a particular combustor.

## BRIEF DESCRIPTION OF THE DRAWINGS

### [0009]

Figure 1 is a schematic of a fuel cell system in accordance with the present invention;  
Figure 2 is a sectioned side view of a combustor in accordance with the present invention;  
Figure 3 is a view in the direction 3-3 of Figure 2;  
Figure 4 is a view in the direction 4-4 of Fig 2;  
Figure 5 is a view in the direction 5-5 of Fig 2; and  
Figure 6 is an isometric view of the heat exchanger of Figure 2.

## DESCRIPTION OF THE PREFERRED EMBODIMENT

[0010] The invention is hereafter described in the context of a fuel cell fueled by reformed methanol (MeOH). However, it is to be understood that the principles embodied herein are equally applicable to fuel cells fueled by other endothermically reformable fuels such as ethanol or gasoline.

[0011] Figure 1 is a schematic of a fuel cell system including a reformer 2 for catalytically reacting methanol from methanol stream 6 and water from water stream 8 to form a hydrogen-rich reformat gas stream 10. The

reformat output gas stream 10 comprises primarily  $H_2$  and  $CO_2$ , but also includes  $N_2$ , CO and water. The reformat stream 10 passes through a shift reactor 12, and a preferential oxidation (PROX) reactor 14, as are well known in the art, to reduce the CO-levels therein to acceptable levels (i.e., below 20 ppm). The CO-purged reformat 10' is then fed into the anode chamber of fuel cell 16. At the same time, oxygen (e.g., air) from oxidant stream 18 is fed into the cathode chamber of the fuel cell 16. The hydrogen from the reformat stream 10 and the oxygen from the oxidant stream 18 react in the fuel cell 16 to produce electricity. Exhaust or effluent 20 from the anode side of the fuel cell contains some unreacted hydrogen. The exhaust or effluent 22 from the cathode side of the fuel cell contains some unreacted oxygen. Air for the oxidant stream 18 is provided by a compressor 24 and is directed to the fuel cell by a valve 26 under normal operating conditions. During startup, however, the valve 26 is rotated to provide air to the input of a combustor 28 used to heat the reformer 2, as will be described in more detail hereinafter.

[0012] The reformer 2 is associated with a heat exchanger 30 such that heat from the heat exchanger 30 heats the catalyst bed in the reformer 2. In this regard, the  $H_2O$ -MeOH mixture inputted to the reformer will be vaporized and preferably be recirculated/refluxed several times (e.g., 20 X) through both the catalyst bed in the reformer 2 and the heat exchanger 30 such that the mixture also functions as a heat transfer medium for carrying heat from the exchanger 30 into the catalyst bed of the reformer 2. The heat exchanger 30 itself is heated from exhaust gases 32 exiting a catalytic combustor 28. The gases 34 exiting the heat exchanger 30 are still hot and pass through an expander 36 which is used to drive a compressor 24 via a drive shaft 38 before being dumped to the atmosphere 40. A shunt valve 42 permits bypassing the heat exchanger 30 and dumping the combustion gases 32 to the expander 36 when the reformer 2 does not require as much heat.

[0013] During normal operation (i.e., after the system has started up and is running), the combustor 28 is fueled by methanol vapor 44, or anode effluent 20 or both, each fed into an input end 46 of the combustor 28. The MeOH vapor 44 emanates from a vaporizer nested in the exhaust end 48 of the combustor 26. The vaporizer is a heat exchanger that extracts heat from the combustor exhaust to vaporize liquid MeOH 50 provided to the heat exchanger from the vehicle's fuel tank. The MeOH vapor 44 exiting the vaporizer and the anode effluent 22 are reacted in a catalyst section 52 of the combustor 28 lying intermediate the input and exhaust ends 46 and 48 respectively of the combustor 28. Oxygen is provided to the combustor either from the cathode effluent stream 22 or a compressor 24 (i.e., via valve 26) depending on whether or not the system is operating under startup conditions with compressor air, or post-startup conditions with cathode effluent. A valve 54 permits dumping the cathode effluent 22 to the

atmosphere 40 via expander 36 when it is not needed in the combustor 28.

[0014] Figure 2 is a side sectional view of a preferred combustor 56, in accordance with the present invention. The combustor 56 comprises a cylindrical metal housing 58 which is lined with two layers of insulating material 60 and 62. A preferred insulating material 60 comprises 0.180 inch thick layers of a ceramic material provided by the 3M company under the tradename INTERAM Mat Material. The combustor 56 has an input end 64 for receiving the combustor fuels and oxidants and an exhaust end 66 through which hot combustor exhaust gas is discharged from the combustor 56 into the heat exchanger 30 associated with the reformer 2 of Figure 1. The exhaust end 66 includes a flange 68 for mounting to the input of the heat exchanger 30 of Figure 1. A primary catalyst bed 70 is positioned between the input end 64 and exhaust end 66 for burning the fuel-oxidant reactants and preferably comprises a catalyst-coated extruded ceramic monolith type bed having about 400 cells per inch at the inlet face 72. Such beds are commonly used in automobile catalytic converters. The bed 70 could be broken into two or more sections/stages each separated from the next and each with a different porosity profile if so desired. A preferred catalyst comprises platinum, but other precious metals, or combinations thereof, may also be used depending on the performance requirements for the combustor. A catalyzed ceramic light-off foam 74 having a porosity profile of about 10 pores per inch and a thickness of about 0.79 inch is provided at the leading face 72 of the monolithic catalyst bed 70. The light-off foam 74 may comprise platinum on a silicon carbide foam substrate, and serves to light-off the reactants prior to their entering the catalyst bed 70, and also provides a tortuous path for mixing the reactants and promoting turbulent oxidation reactions.

[0015] A turbulator section T precedes the light-off foam 74 and comprises at least one porous bed of mixing media upstream of the light-off catalyst 74 which provides a tortuous path therethrough to promote turbulent flow, and intimate mixing of the combustor fuel(s) and air before they contact the light-off catalyst 74. The turbulator section T will preferably comprise at least two mixing-media beds 76 and 80 with an open chamber 82 between the mixing-media beds to act as a homogenization region for homogenizing the mixture exiting the first mixing-media bed 80 before it enters the second mixing-media bed 76. The mixing-media beds 76 and 80 have leading faces 77 and 81 respectively where the reactants enter the beds and trailing faces 79 and 83 respectively where the reactants exit the beds 76 and 80. Preferred mixing media comprises ceramic foams having a porosity profile of about 25 pores per lineal inch to about 80 pores per lineal inch, but other materials and porosity profiles may be used. A preferred mixing-media for bed 76 comprises silicon carbide foam having a porosity profile of about 25 pores per linear

inch and a thickness of about one inch. Alternative mixing-media beds include refractory metal foams, ceramic pellets retained in a flow-through container, or a stack of fine (e.g., about 0.001 to about 0.010 openings per inch) metal or ceramic screens, wherein the openings of one screen are offset from the openings in adjacent screens to provide the desired tortuous path. The mixing-media bed 76 can also function as a flame suppressor to prevent any flame created at the light-off catalyst 74 from propagating back into the input end 64 of the combustor 56, and as a means to distribute the reaction mixture evenly across the leading face 72 of the catalyst bed 70.

[0016] An electric heating element 78 is provided upstream of the mixing media 76 and serves to vaporize liquid fuel entering the combustor 56, and to heat the gas entering the catalyst bed 70 during initial startup of the combustor 56. The heating element 78 may or may not be catalyzed, and is energized by electrical contacts 85 and 85' (Figure 4) which are provided with electricity via electrical leads 104 and 104'. After startup, the electric heater 78 is no longer required since the fuel will be vaporized by the exhaust gases emanating from the exhaust end 66 of the combustor 56, as will be discussed in more detail hereinafter. A preferred electric heater 78 comprises a commercially available, uncatalyzed extruded metal monolith resistance element such as is used to light off the catalyst of a catalytic converter used to treat IC engine exhaust gases.

[0017] Another mixing-media bed 80 of the turbulator section T lies upstream of the electric heater 78. The mixing-media 80 provides a tortuous path therethrough and induces turbulent flow for mixing the reactants before they contact the electric heater 78. The heater 78 resides in the homogenization space 82 that lies between the mixing-media beds 76 and 80 and further serves to promote mixing of the reactants exiting the first stage mixing media 80 prior to their entering the second stage mixing media 76. This first stage mixing media preferably has a smaller pore size than the second stage mixing media 76. A suitable turbulator first stage mixing media 80 comprises a ceramic foam comprising yttria-zirconia-alumina having a porosity profile of about 80 pores per linear inch and a thickness of about 0.375 inch. The mixing media 80 additionally serves as a flame arrestor to suppress any flame that might result from fuel ignited by the electric heating element 78, or down stream catalyst bed, from propagating back into the mixing chamber 84 where the reactants mix before passing through the mixing media 80.

[0018] H<sub>2</sub>-containing anode effluent 20 (see Figure 1) exiting the anode side of the fuel cell 16 enters the input end 64 of the combustor 56 via the annular plenum 86 that surrounds the shell 94 that contains the mixing media 80, and passes through a porous, metal disc 88 into the mixing chamber 92. The disc 88 may or may not be cooled (e.g., with water) and serves to diffuse the H<sub>2</sub> therethrough while functioning as a flame arrestor against flame entering into the plenum 86. The flame

arrestor 88 will preferably comprise a sintered metal disk having a pore size of about 40 microns, and a thickness of about 0.078 inch. O<sub>2</sub>-containing cathode effluent 22 (see Figure 1) exiting the cathode side of the fuel cell 16 enters the input end 64 of the combustor 56, via conduit 90, and swirls in the annular chamber 92 defined centrally by the shell 94. In the chamber 92 the swirling cathode effluent picks up, and to some extent mixes with, the anode effluent passing through the flame arrestor 88. A suitable insulating material 96 similar to the insulating material 60 and 62 lines the shell 94 containing the mixing media 80. A narrow annular gap 98 (i.e., about 3.0 mm) between the leading edge 95 of the shell 94 and the end wall 100 of the housing 58 insures that some degree of mixing of the cathode and anode effluents occurs in the chamber 92 before they move into the input chamber 97, which is a vestibule to the mixing media 80.

[0019] The exhaust end 66 of the combustor 56 includes a chamber 106 that houses a heat exchanger 108 which, in the embodiment shown, comprises a coil of metal tubing 110. (See Figure 6). The heat exchanger 108 is used to vaporize liquid fuel used to fuel the combustor 56. More specifically, under normal post-startup conditions, air or cathode effluent 22 (see Figure 1) may be introduced into the inlet end 114 of the coil 110 and mixed with liquid fuel sprayed into the input end 114 via a conventional automotive type fuel injector 116. The airborne atomized fuel passes through the several turns of the heated coil tube 110, and therein vaporizes and exits the heat exchanger 108 at outlet 118 which is located in the cathode effluent supply conduit 90. This vaporized fuel supplements the anode effluent 20 (see Figure 1) as fuel for the combustor 56 as may be needed to meet the transient and steady state needs of the fuel cell system. The vaporizer coil 110 is sized to vaporize the maximum flow rate of fuel with the minimum combustor exhaust flow rate, and is designed to operate at temperatures exceeding the autoignition temperature of the MeOH-air mixture therein throughout its full operational range. Autoignition within the vaporizer is avoided, however, by insuring that the velocity of the mix flowing through the coil 110 significantly exceeds the worst-case flame speed of the mixture which varies with the composition of the inlet streams. For stoichiometric mixtures at atmospheric pressure, this speed would be 0.48 meters per sec. Hot combustion gases exiting the catalyst bed 70 contact the heat exchanger coil 110 for heating fluid flowing through the interior or the coiled tube 110. A pipe 112 coupled to the chamber 106 permits the diversion of any excess hot combustor exhaust gases from the chamber 106 which are not needed to heat the reformer. These diverted excess gases may conveniently be shunted to the expander 36 via valve 42 (see Figures 1).

[0020] The fuel cell system of the present invention operates as follows. At the beginning of operations when the system is cold and starting up: (1) the com-

pressor 24 (Figure 1) is driven by an electric motor energized from an external source (e.g., a battery) to provide the necessary system air; (2) air is introduced into conduit tube 90 as well as the input end 114 of the tubular heat exchanger 110; (3) liquid fuel (e.g., MeOH) is injected into the inlet end 114 of the tubular heat exchanger 110 via fuel injector 116, and admixed as fine droplets with the air flowing therein; (4) the air-MeOH droplet mix exits the now cold coil 110 at outlet 118 and mixes with compressor air introduced into conduit 90, and is then introduced into the annular chamber 92 in the input end 64 of the combustor 56; (5) the mix passes through the first mixing-media bed 80 of the turbulator section; (6) the mix exiting the mixing-media bed 80 is heated by the heater 78 in the homogenization chamber 82 to vaporize the liquid droplets and heat the mixture; (7) the preheated vaporous mix then enters the mixing-media bed 76 for still further intimate mixing before contacting the light-off catalyst bed 74; (8) upon exiting the mixing-media bed 74, the mix begins oxidizing on the light-off catalyst bed 74 just before it enters the primary catalyst bed 70, or reacting section of the combustor 56, where substantially complete combustion of the fuel is effected; and (9) the hot exhaust gases exiting the catalyst bed 70 are conveyed to the heat exchanger 30 associated with the reformer 2 (Figure 1). Once the reformer's temperature has risen sufficiently to effect and maintain the reformation process: (1) valve 26 is rotated to direct air to the cathode side of the fuel cell 16 (Figure 1); (2) MeOH and water are fed to the reformer 2 to commence the reformation reaction; (3) reformate exiting the reformer 2 is fed to the anode side of the fuel cell 16; (4) anode effluent 20 from the fuel cell 16 is directed into plenum 86 of the combustor 56; (5) cathode effluent 22 from the fuel cell 16 is directed into annular chamber 92 of the combustor 56; (6) air is introduced into the inlet 114 of the tubular heat exchanger 110; (7) liquid methanol is sprayed into the inlet 114 by the injector 116; (8) the methanol-air mix circulates through the heated tubular heat exchanger coil 110 where the MeOH vaporizes; (9) the Air-MeOH<sub>(v)</sub> mix exits the heat exchanger at outlet 118 and is fed into the chamber 92 along with the cathode effluent 22 where it mixes with the anode effluent passing through the flame arrestor 88 from plenum 86; and (10) the mix passes into the turbulator section of the combustor for burning on the catalyst bed 70 as discussed above in connection with the start-up mode. During normal (i.e., post startup) operating conditions, the heater 78 is not used as the heat exchanger coil 110 alone vaporizes the MeOH and preheats the MeOH-air mix. Under certain conditions, the combustor 56 could operate solely on the anode and cathode effluents alone, without the need for additional MeOH fuel from the heat exchanger 110. Under such conditions, MeOH injection through injector 116 is discontinued. Under other conditions, e.g., increasing power demands, supplemental fuel is provided to the combustor via the injector 116. More

such supplemental fuel will be needed in the future as stack fuel efficiencies increase and the H<sub>2</sub> content of the anode effluent 20 and O<sub>2</sub> content of the cathode effluent 22 is reduced.

[0021] While the invention has been described primarily in terms of a specific embodiment thereof it is not intended to be limited thereto but rather only to the extent set forth hereafter in the claims which follow.

#### Claims

1. In a fuel cell system comprising essentially (a) a stack of H<sub>2</sub> - O<sub>2</sub> fuel cells discharging an H<sub>2</sub> -containing anode effluent and an O<sub>2</sub> -containing cathode effluent, (b) a fuel reformer for converting a hydrogen-containing fuel selected from the group consisting of alcohols and hydrocarbons to H<sub>2</sub> for fueling said cells, and (c) a combustor for heating said fuel reformer, the improvement comprising:  
 said combustor being fueled by said anode and cathode effluents and comprising a housing having an input chamber receiving and combining said anode and cathode effluents together into a burnable mixture, an exhaust outlet emitting hot combustor exhaust gas to said reformer, a catalyst bed intermediate said chamber and said exhaust outlet for burning said mixture to generate said combustor exhaust gas, and a turbulator intermediate said input chamber and said catalyst bed for inducing turbulent mixing of said mixture before it contacts said catalyst bed, said turbulator comprising at least one porous bed having a leading face admitting said mixture into said porous bed from said input chamber and a trailing face through which said mixture exits said porous bed and a mixing zone intermediate said leading and trailing faces for intimately mixing said effluents in said mixture, said mixing zone defining a multiplicity of tortuously pathed channels through which said mixture passes.
2. A system according to claim 1 wherein said turbulator comprises first and second said porous beds arranged in series between said chamber and said catalyst bed.
3. A system according to claim 2 wherein said porous beds have different porosity profiles.
4. A system according to claim 3 wherein said first porous bed in the direction of flow has a finer porosity profile than said second porous bed.
5. A system according to claim 2 wherein said porous beds are separated one from the other by an open space.

6. A system according to claim 1 wherein said porous bed comprises a stack of screens wherein the openings in one screen are offset from openings in adjacent screens to provide said tortuous path through said porous bed.
7. A system according to claim 1 wherein said porous bed comprises a material selected from the group consisting of ceramics and refractory metals.
8. A system according to claim 7 wherein said material comprises an open cell foam.

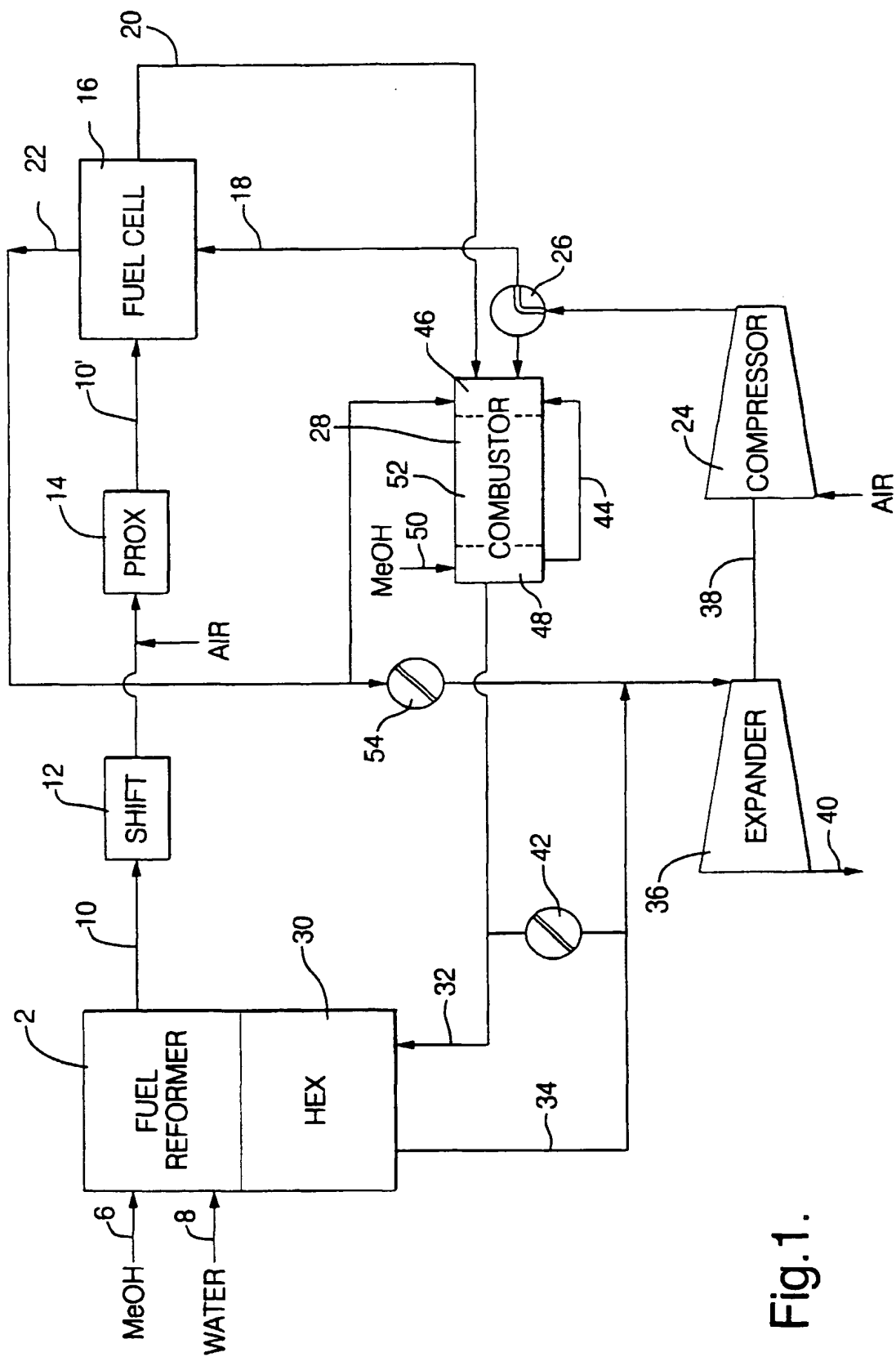


Fig.1.

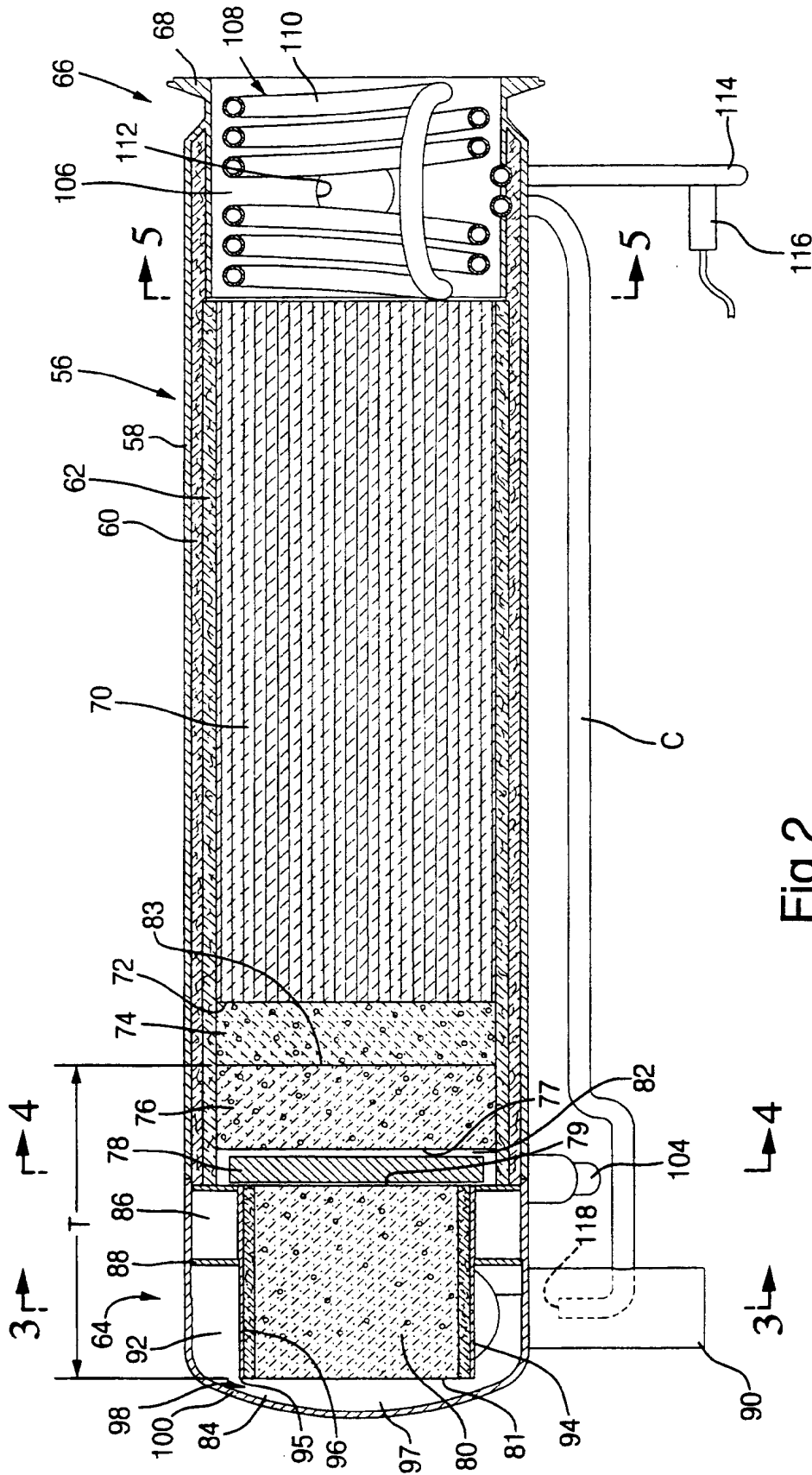


Fig. 2.



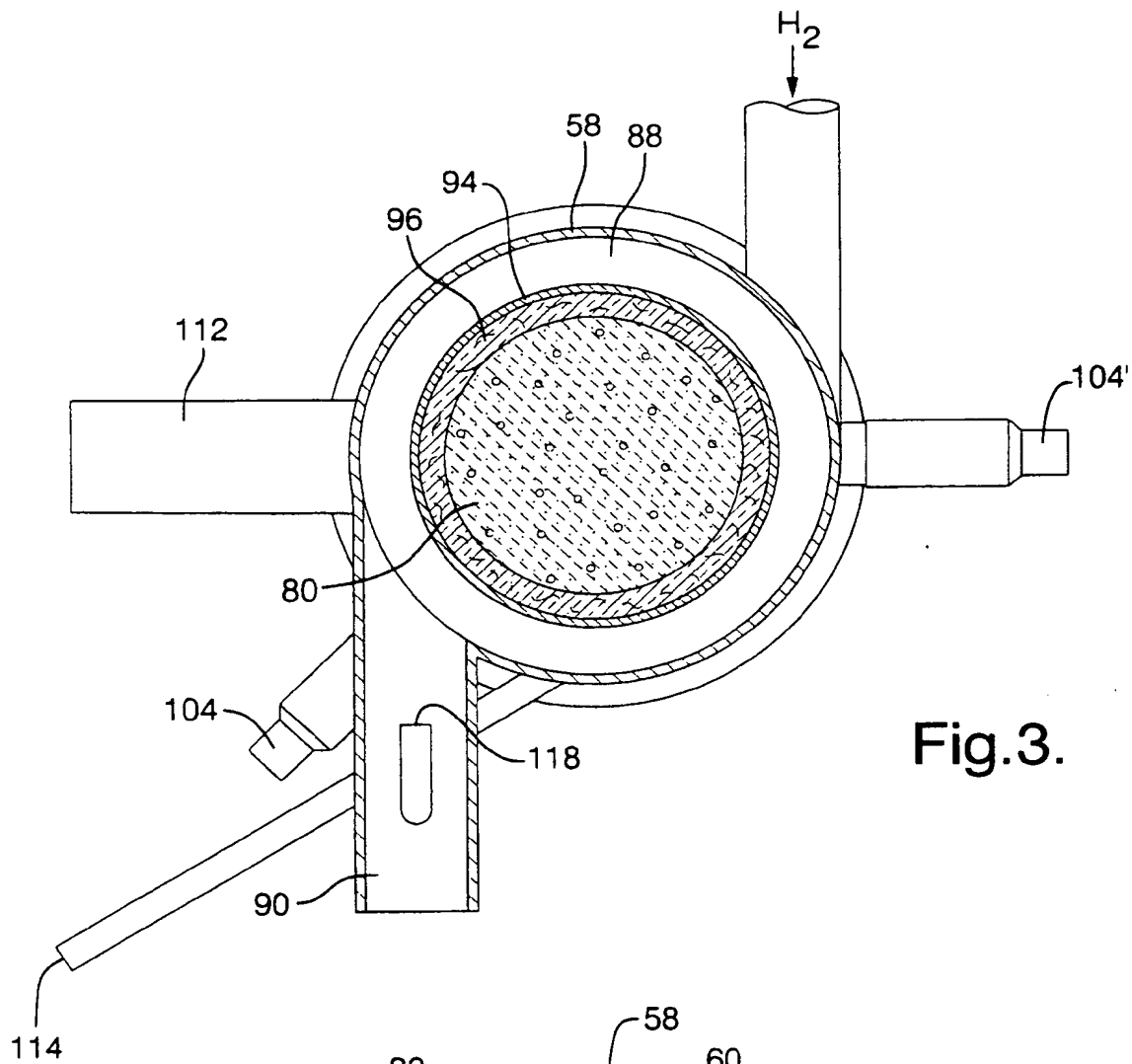


Fig.3.

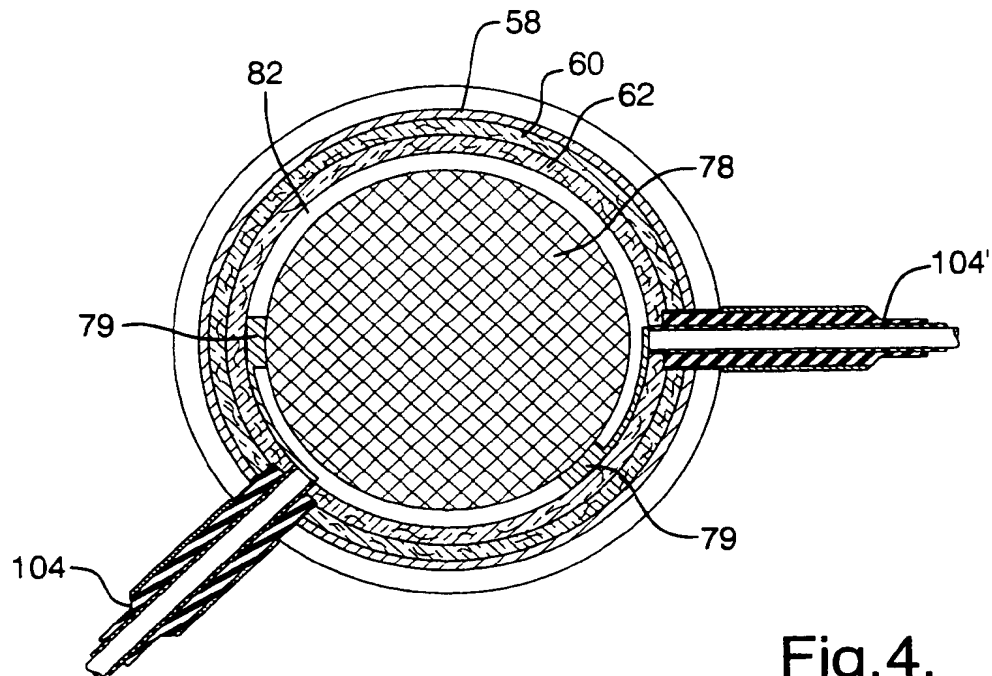


Fig.4.

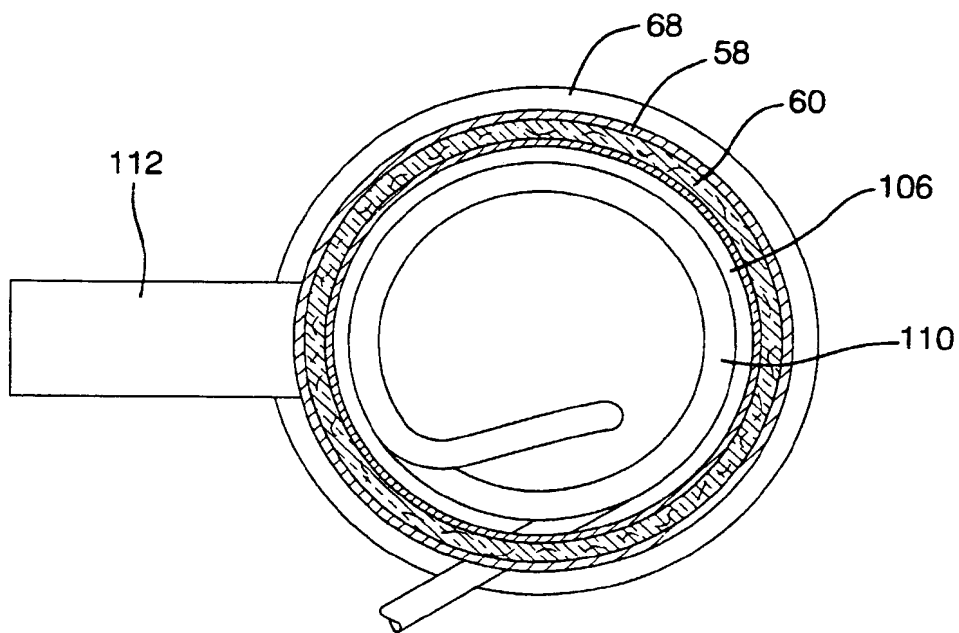


Fig.5.

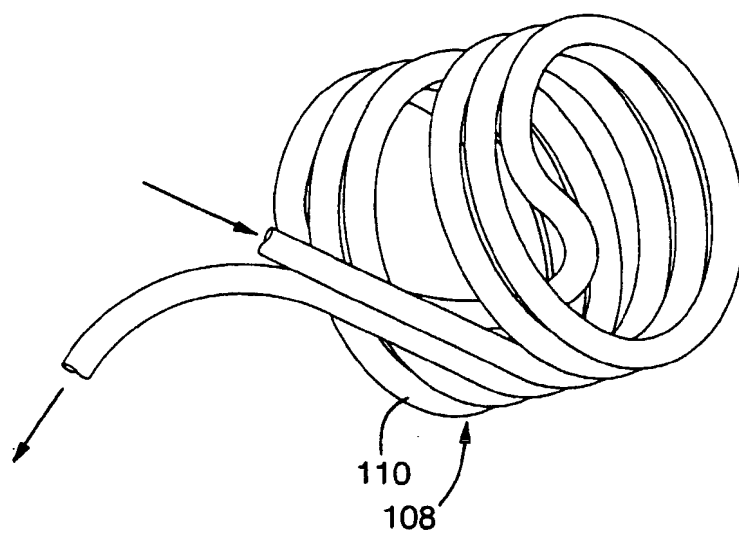
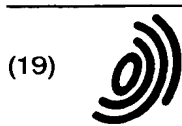


Fig.6.



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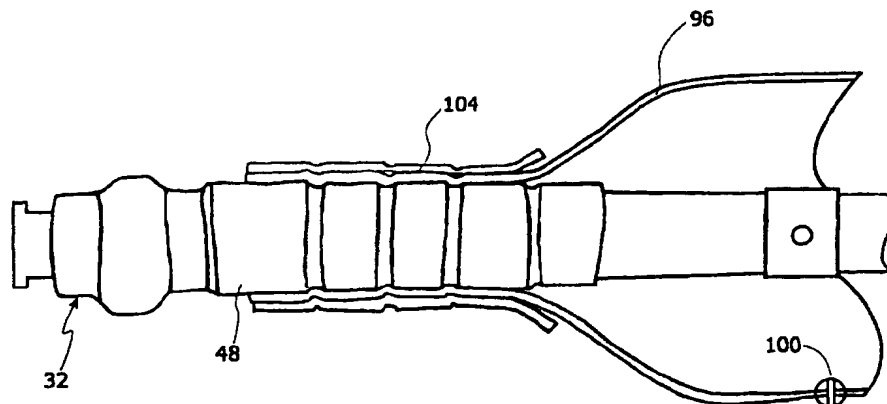
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(54) **Fuel cell system combustor**

(57) A fuel cell system including a fuel reformer heated by a catalytic combustor fired by anode and cathode effluents. The combustor includes a turbulator section (T) at its input end for intimately mixing the anode and cathode effluents before they contact the combustors primary catalyst bed (70). The turbulator

comprises at least one porous bed (76,80) of mixing media that provides a tortuous path therethrough for creating turbulent flow and intimate mixing of the anode and cathode effluents therein.



**FIG. 2**



European Patent  
Office

# EUROPEAN SEARCH REPORT

Application Number  
EP 98 20 2160

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
X	JP 01 136236 U (FUJI ELECTRIC CO) 19 September 1989 (1989-09-19) * the whole document *	1-3	H01M8/06 H01M8/04 F23D14/18
X	PATENT ABSTRACTS OF JAPAN vol. 016, no. 335 (M-1283), 21 July 1992 (1992-07-21) -& JP 04 098011 A (YOUYUU TANSANENGATA NENRIYOU DENCHI HATSUDEN SHISUTEMU GIJIYUTSU KENKI), 30 March 1992 (1992-03-30) * abstract *	1,2,5,7	
A	PATENT ABSTRACTS OF JAPAN vol. 013, no. 592 (C-671), 26 December 1989 (1989-12-26) & JP 01 249890 A (BABCOCK HITACHI KK), 5 October 1989 (1989-10-05) * abstract *	1,2,5,7, 8	
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The present search report has been drawn up for all claims			
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EPO FORM 1503 03.02 (P/04031)



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Application Number  
EP 98 20 2160

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CATEGORY OF CITED DOCUMENTS		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons ..... & : member of the same patent family, corresponding document	
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